

Description

Method and apparatus for controlling an internal combustion engine

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The invention relates to a method and apparatus for controlling an internal combustion engine with an intake tract and an exhaust tract incorporating a three-way catalytic converter, and with at least one cylinder which communicates with the intake tract depending on the position of a gas inlet valve and which communicates with the exhaust tract depending on the position of a gas outlet valve. There is additionally assigned to the at least one cylinder an injection valve which meters fuel in. An oxygen sensor is disposed downstream of the three-way catalytic converter in the exhaust tract.

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For internal combustion engines, increasingly stringent statutory provisions make it necessary on the one hand to reduce as much as possible the raw emissions caused by the combustion of the air/fuel mixture in the relevant cylinder. On the other hand, exhaust aftertreatment systems are employed in internal combustion engines to convert the pollutant emissions produced during the combustion process of the air/fuel mixture in the cylinder into harmless substances. Specifically in the case of gasoline engines a three-way catalytic converter located in the engine's exhaust tract is used for this purpose. A high degree of efficiency in the conversion of the pollutant components carbon monoxide, hydrocarbons and nitrogen oxides is only guaranteed in a very narrow window between the stoichiometric air/fuel ratio and approximately 6 tenths of a percent in the direction of excess fuel. To compensate for actual variations in the air/fuel ratio in the relevant cylinder, three-way catalytic converters are coated with a layer of material which can briefly store

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oxygen and bind or release it as required. Such a coating is known as a washcoat and consists e.g. of Ce_2O_3 (dicerium trioxide). By means of this washcoat, fluctuations in the air/fuel mixture and the corresponding exhaust gas are thus compensated in the catalytic converter as long as the washcoat has not yet bound its maximum quantity of oxygen or else no more oxygen is bound in the washcoat. However, if these limits are exceeded, the efficiency of the three-way catalytic converter is markedly reduced, resulting in increased pollutant emissions from the internal combustion engine.

In the case of closed-loop lambda control incorporating an oxygen sensor disposed upstream of the three-way catalytic converter, it is known to use the measurement signal of an oxygen probe which is disposed downstream of the three-way catalytic converter and generates a binary measurement signal, to adjust a P- or I-component of the control parameters or a delay time of the lambda controller accordingly as a function of the measurement signal of the oxygen sensor downstream of the three-way catalytic converter. This is also known as trim control. However, it has been found that, despite this measure, particularly in the case of aging three-way catalytic converters, undesirably high pollutant emissions of the internal combustion engine may continue to occur.

The object of the invention is to create a method and an apparatus for controlling an internal combustion engine which ensure low pollutant emissions over a long operating period of the internal combustion engine in a simple manner.

This object is achieved by the features of the independent claims. Advantageous embodiments of the invention are set forth in the dependent claims.

In respect of a first aspect, the invention is characterized by a method and a corresponding apparatus for controlling an internal combustion engine, wherein a mass of fuel to be supplied, which is to be fed to the relevant cylinder, is
5 determined as a function of a load variable. The load variable can be, for example, a mass air flow into the relevant cylinder, but can equally be any other load variable such as a torque to be produced by the internal combustion engine which is determined e.g. as a function of the position of an
10 accelerator pedal or some other means.

An additional mass of fuel to be metered-in on a one-time basis is determined if the measurement signal of a post-cat oxygen sensor disposed downstream of a three-way catalytic
15 converter in an exhaust tract of the internal combustion engine is characteristic of at least one predefined residual oxygen component. The additional mass of fuel is in this case determined as a function of the response of the measurement signal of the post-cat oxygen sensor. A corrected mass of fuel
20 to be supplied is determined as a function of the mass of fuel to be supplied and if necessary the mass of fuel to be metered-in on a one-time basis. An actuating signal for controlling the injection valve is generated as a function of the corrected mass of fuel to be supplied. The one-time mass
25 of fuel to be metered-in can either be metered-in within one operating cycle of a cylinder or else spread over several operating cycles of the cylinder. The invention uses the knowledge that when the measurement signal of the post-cat oxygen sensor is characteristic of at least one predefined
30 residual oxygen component, the three-way catalytic converter essentially cannot store any more additional oxygen and thus during operation of the internal combustion engine in this state, even if a known trim control may be present, a so-called breakthrough of the measurement signal of the post-cat

oxygen sensor frequently occurs again and again with associated pollutant emissions, in particular NOX emissions of the internal combustion engine.

- 5 By the metering-in of the mass of fuel to be metered-in on a one-time basis, the three-way catalytic converter is placed in a state in which an appropriately predefinable reserve is provided for absorbing or storing oxygen, thereby enabling corresponding fluctuations in the air/fuel ratio in cylinders
10 to be very well compensated by the three-way catalytic converter and quickly ensuring a significant reduction in pollutant emissions.

- In this connection the mass of fuel to be metered-in on a one-
15 time basis can be determined in a particularly simple manner if the measurement signal of the post-cat oxygen sensor falls below a specified first threshold value, the specified first threshold value being suitably predefined.

- 20 According to an advantageous embodiment of the invention, the mass of fuel to be metered-in on a one-time basis is predefined such that approximately 50 % of the oxygen storable in the three-way catalytic converter remains after metering-in of the mass of fuel to be metered-in on a one-time basis. In
25 this way, after metering-in of the mass of fuel to be metered-in on a one-time basis, a maximum variability of the air/fuel ratio in the relevant cylinder is possible without any increase in pollutant emissions downstream of the three-way catalytic converter.

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According to another advantageous embodiment of the invention, the mass of fuel to be metered-in on a one-time basis is determined from an estimated value of the current oxygen storage capacity by means of a physical model of the three-way

catalytic converter. In this way, the stored oxygen remaining in the three-way catalytic converter after metering-in of the mass of fuel to be metered-in on a one-time basis can be very precisely adjusted.

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According to another advantageous embodiment of the invention, the mass of fuel to be metered-in on a one-time basis can be determined as a function of a gradient of the measurement signal of the post-cat oxygen sensor. The gradient is a very
10 good indicator of the state of the three-way catalytic converter and therefore as to whether a slight or severe oxygen overflow is present. In this way, the stored oxygen remaining in the three-way catalytic converter after metering-in of the mass of fuel to be metered-in on a one-time basis
15 can be very precisely adjusted.

According to another advantageous embodiment of the invention, the mass of fuel to be metered-in on a one-time basis is determined as a function of a minimum measured value of the
20 measurement signal, while the measurement signal of the post-cat oxygen sensor is characteristic of at least one predefined residual oxygen component. The minimum measured value is a very good indicator of the state of a three-way catalytic converter and therefore as to whether a slight or severe
25 oxygen overflow is present. In this way, the stored oxygen remaining in the three-way catalytic converter after metering-in of the mass of fuel to be metered-in on a one-time basis can be very precisely adjusted.

30 According to a second aspect, the invention is characterized by a method and a corresponding apparatus wherein a mass of fuel to be supplied to the cylinder is determined as a function of a load variable, and a mass of fuel reduced on a one-time basis is determined if the measurement signal of the

post-cat oxygen sensor is characteristic of at least one predefined residual fuel component, namely as a function of the response of the measurement signal.

5 A corrected mass of fuel to be supplied is determined as a function of the mass of fuel to be supplied minus if necessary the mass of fuel reduced on a one-time basis. An actuating signal for controlling the injection valve is generated as a function of the corrected mass of fuel to be supplied, using
10 the knowledge that, when the measurement signal of the post-cat oxygen sensor is characteristic of at least one predefined residual fuel component, the three-way catalytic converter has essentially stored no more oxygen and thus during operation of the internal combustion engine in this state, even if a known
15 trim control may be present, a so-called breakthrough of the measurement signal of the post-cat oxygen sensor frequently occurs again and again with associated pollutant emissions, in particular CO and HC emissions of the internal combustion engine.

20 By means of the mass of fuel reduced on a one-time basis, with suitable selection of same a corresponding oxygen excess, relative to the stoichiometric air/fuel ratio, can be produced which then results in a corresponding storage of oxygen in the
25 three-way catalytic converter. There is then provided in the three-way catalytic converter a correspondingly predefinable reserve for absorbing or storing oxygen. This enables corresponding fluctuations of the air/fuel ratio in cylinders to be very well compensated by the three-way catalytic
30 converter and a substantial reduction in pollutant emissions is quickly ensured.

In an advantageous embodiment of the second aspect of the invention, the mass of fuel reduced on a one-time basis is

determined if the measurement signal of the post-cat oxygen sensor exceeds a predefined second threshold value. This is particularly simple.

5 According to a further advantageous embodiment of this aspect of the invention, the mass of fuel reduced on a one-time basis is predefined such that approximately 50 % of the oxygen storable in the three-way catalytic converter is stored after a mass of fuel, less the reduced mass of fuel, has been
10 correspondingly metered-in.

According to another advantageous embodiment of the second aspect of the invention, the estimated value of the current oxygen storage capacity of the three-way catalytic converter
15 is determined.

According to another advantageous embodiment of the second aspect of the invention, the mass of fuel reduced on a one-time basis is determined as a function of the gradient of the
20 measurement signal of the post-cat oxygen sensor.

According to another advantageous embodiment of the second aspect of the invention, the mass of fuel reduced on a one-time basis is determined as a function of a maximum value of
25 the measurement signal while the measurement signal of the post-cat oxygen sensor is characteristic of at least one predefined residual fuel component.

Exemplary embodiments of the invention are explained in
30 greater detail below with reference to the accompanying schematic drawings, in which:

Figure 1 shows an internal combustion engine with a control device,

Figure 2 shows a block diagram of the control device,

Figure 3 shows a flowchart of a first part of a program for
controlling an internal combustion engine, and

Figure 4 shows a second part of a program for controlling the
internal combustion engine.

In the figures, constructionally or functionally identical
elements are denoted by the same reference numerals
throughout.

An internal combustion engine (Figure 1) comprises an intake
tract 1, an engine block 2, a cylinder head 3 and an exhaust
tract 4. The intake tract 4 preferably incorporates a throttle
valve 6, as well as a plenum 7 and an intake pipe 8 which
leads to a cylinder Z1 via an intake duct in the engine block
2. The engine block 2 additionally comprises a crankshaft 10
which is coupled to the piston 12 of the cylinder Z1 via a
connecting rod 11.

The cylinder head 3 contains a valve train comprising a gas
inlet valve 14, a gas outlet valve 15 and valve operating
mechanisms 16, 17. The cylinder head 3 additionally
incorporates an injection valve 19 and a spark plug 20.
Alternatively, the injection valve 19 can also be disposed in
the intake pipe 8.

The exhaust tract 4 incorporates a catalytic converter 22
which is implemented as a three-way catalytic converter.

A control device 24 is provided to which sensors are assigned
which detect different measured variables and determine the

measured value of the measured variable in each case. As a function of at least one of the measured variables, the control device 24 determines manipulated variables which are then converted into one or more actuating signals for
5 controlling the actuators by means of corresponding servo drives.

The sensors are a pedal position transducer 25 which detects a position of the accelerator pedal 26, a mass air flow meter 28
10 which detects a mass air flow upstream of the throttle valve 6, a temperature sensor 32 which measures the intake air temperature, a crankshaft angle sensor 34 which detects a crankshaft angle to which a speed N is assigned, a post-cat oxygen sensor 37 which is disposed downstream of the three-way
15 catalytic converter 22 and which detects a residual oxygen component of the exhaust gas downstream of the three-way catalytic converter 22. Depending on the residual oxygen content, a measurement signal MS which is preferably a voltage signal is fed out to the control device. There is additionally
20 provided a pre-cat oxygen sensor 36 whose measurement signal is characteristic of an air/fuel ratio in the cylinder Z1. A subset of the abovementioned sensors can be present or additional sensors can also be present depending on the embodiment of the invention.

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The actuators are e.g. the throttle valve 6, the gas inlet and gas outlet valves 14, 15, the injection valve 19 or the spark plug 20.

30 In addition to the cylinder Z1, other cylinders Z2 to Z4 are also provided to which corresponding actuators are also then assigned.

A block diagram of the control device 24, which may also be termed an apparatus for controlling the internal combustion engine, is shown in Figure 2. The relevant blocks of the control device 24 in the context of the invention are
5 illustrated in the block diagram.

A dashed-line block B1 corresponds to the internal combustion engine according to Figure 1. From the measurement signal of the pre-cat oxygen sensor 36 an actual air/fuel ratio LAM_AV
10 in the cylinder Z1 - Z4 is obtained and fed to a block B2. The pre-cat oxygen sensor 36 is preferably implemented as a linear lambda probe but can also be implemented as a simple binary lambda probe whose measurement signal has a lean value if the air-fuel ratio in the cylinder Z1 - Z4 is greater than a
15 stoichiometric air/fuel ratio and whose measurement signal has a rich value if the air/fuel ratio in the cylinder Z1 - Z4 is less than the stoichiometric air/fuel ratio. To the block B2 there is additionally fed a setpoint air/fuel ratio LAM_SP which is to be set in the cylinder Z1 - Z4. The setpoint
20 air/fuel ratio LAM_SP preferably has approximately the value of the stoichiometric air/fuel ratio. However, particularly in the case of a linear lambda probe, it can also be provided with forced excitation and thus vary cyclically about the stoichiometric value.

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The difference between the setpoint and actual air/fuel ratio LAM_SP, LAM_AV is fed to a closed-loop controller which is implemented in the block B2. The controller has an integral control parameter and a proportional control parameter and is
30 implemented as a lambda controller known to the average person skilled in the art. The manipulated variable of the controller in the block B2 is a lambda control factor LAM_FAC.

In a block B4, a mass of fuel to be metered-in MFF is determined as a function of a load variable, preferably a mass of air MAF in the relevant cylinder Z1 - Z4 of the internal combustion engine and a speed N of the crankshaft. The mass of
5 air MAF in the relevant cylinder Z1 - Z4 is preferably determined by means of a physical model as a function of the throttle valve position determined by the throttle valve position sensor 30, the speed N and possibly other variables such as the intake pipe pressure or the detected mass air flow
10 upstream of the throttle valve.

Alternatively, however, the load variable can also be another variable such as a torque to be produced by the internal combustion engine which is preferably determined as a function
15 of the accelerator pedal position and possibly other variables.

There is additionally provided a block B8 to which the measurement signal MS of the post-cat oxygen sensor 37 is fed.
20 In the block B8 there is determined if necessary, as a function of the measurement signal MS of the post-cat oxygen sensor 37, a mass of fuel to be metered-in on a one-time basis MFF_ADD or a mass of fuel reduced on a one-time basis MFF_RED. For this purpose there is executed in the block B8 a program
25 which will be explained in greater detail below with reference to Figures 3 and 4.

A corrected mass of fuel to be metered-in MFF_COR is determined in a block B5 by means of a corrected mass of fuel
30 to be supplied MFF_COR by multiplying the lambda control factor LAM_FAC by the sum of or difference between the mass of fuel to be metered-in and the mass of fuel to be metered-in on a one-time basis or rather the mass of fuel reduced on a one-time basis MFF_RED. Alternatively, in the block B5, the

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product of the mass of fuel to be metered-in MFF and the lambda control factor LAM_FAC can also be added to the mass of fuel to be metered-in on a one-time basis or rather the mass of fuel reduced on a one-time basis MFF_RED.

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In a block B6, depending on the corrected mass of fuel to be metered-in MFF_COR, an actuating signal SG for the injection valve(s) 19 is generated and the injection valves 19 are actuated accordingly.

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The program executed in the block B8 is initiated in a step S1, preferably contemporaneously with startup of the internal combustion engine. In step S1, variables are preferably initialized, such as a counter i or an additional counter j.

15 The counters i, j preferably assume the value 1.

In a step S2 it is checked whether the current value of the measurement signal MS is less than a predefined first threshold value THD1. The first threshold value THD1 is

20 suitably selected such that it is characteristic of at least one predefined residual oxygen component of the exhaust gas in the region of the post-cat oxygen sensor 37. A binary lambda probe whose measurement signal is preferably a voltage signal is preferably used as post-cat oxygen sensor. The first
25 threshold value is then e.g. approximately 550 mV.

If the condition of step S2 is fulfilled, the current value of the measurement signal MS of the post-cat oxygen sensor 37 is temporarily stored at a memory location for the measurement
30 signal MS which is determined by the value of the counter i. Then in a step S4 the counter i is incremented, preferably by 1.

In a step S6 it is checked whether the counter *i* has a value greater than a minimum counter value *i_min* of the counter *i*. The minimum counter value *i_min* can be e.g. two. If the condition of step S6 is not fulfilled, the program remains in a step S5 for a predefined wait time *T_W* before the condition of step S2 is rechecked.

If the condition of step S6 is fulfilled, in a step S7 a gradient *GRAD_MS* of the measurement signal *MS* of the post-cat oxygen sensor 37 is determined as a function of the temporarily stored values of the measurement signal *MS*. In this context the gradient *GRAD_MS* is taken to mean the variation over time, i.e. the time derivative of the measurement signal *MS*. The gradient *GRAD_MS* can be determined in different ways, for example the gradient may denote the fall over time of the measurement signal *MS* immediately after the first threshold value *THD1* has been undershot and therefore be characteristic of the rate at which the measurement signal *MS* is decreasing. However, it can also be determined as being characteristic of the rate of increase of the value of the measurement signal up to the first threshold value *THD1*.

In a following step S8 a minimum value *MIN_MS* of the measurement signal *MS* of the post-cat oxygen sensor 37 is determined as a function of the temporarily stored values of the measurement signal *MS* of the post-cat oxygen sensor 37.

Then, in a step S10, an estimated value *OSC* of the current oxygen storage capacity of the three-way catalytic converter 22 is determined. Alternatively, the estimated value *OSC* of the current oxygen storage capacity of the three-way catalytic converter 22 can also be determined by another program which is executed in the control device 24, possibly at other times,

- and merely read in in step S10. The estimated value OSC of the current oxygen storage capacity of the three-way catalytic converter 22 is preferably determined by means of a physical model. If necessary forced excitation with an increased
5 amplitude takes place for this purpose, particularly in the case of a linear lambda probe as pre-cat oxygen sensor, in order thus to check and determine the oxygen storage capacity of the three-way catalytic converter 22.
- 10 In a subsequent step S11, the mass of fuel to be metered-in on a one-time basis MFF_ADD is determined as a function of the gradient GRAD_MS of the measurement signal MS of the post-cat oxygen sensor 37 and/or the minimum value MIN_MS of the
15 measurement signal MS of the post-cat oxygen sensor 37 and/or the estimated value OSC of the current oxygen storage capacity of the three-way catalytic converter 22. Preferably this takes place optionally by means of one or more engine maps determined in advance by experiments or even simulations.
- 20 Preferably the mass of fuel to be additionally metered-in MFF_ADD is thus determined in such a way that, after the metering-in of the mass of fuel to be metered-in on a one-time basis MFF_ADD, the oxygen stored in the three-way catalytic converter 22 is approximately 50 % of the maximum amount of
25 oxygen currently storable in the three-way catalytic converter 22. In a particularly simple implementation of the program, the mass of fuel to be metered-in on a one-time basis MFF_ADD can also be permanently predefined.
- 30 In a subsequent step S12, the counter i is re-initialized with the value 1 and processing is then continued in step S5.

If the condition of step S2 is not fulfilled, i.e. the current value of the measurement signal MS is not less than the first

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predefined threshold value THD1, the counter i is re-initialized with the value 1 in a step S14.

Following step S14, processing is continued in a step S15 in
5 which it is checked whether the current measurement signal MS is greater than a predefined second threshold value THD2. The second threshold value THD2 is suitably predefined in such a way that if the measurement signal MS of the post-cat oxygen sensor 37 exceeds the second threshold value THD2, the
10 measurement signal MS is characteristic of at least one predefined residual fuel component of the exhaust gas downstream of the three-way catalytic converter 22.

If the condition of step S15 is not fulfilled, the counter j
15 is initialized in a step S22, preferably with one. Processing is then continued in the step S5.

If the condition of step S15 is fulfilled, in a step S16 the current value of the measurement signal MS of the post-cat
20 oxygen sensor 37 is temporarily stored in a memory location for the measurement signal MS which is determined by the counter j. In a step S18 the counter j is then incremented by the value, preferably by the value 1.

25 In a step S20 it is checked whether the counter j is over a minimum count j_min for the counter j, which is e.g. two. If this is not the case, processing is continued in step S5.

However, if the condition of step S20 is fulfilled, in a step
30 S21 the gradient GRAD_MS of the measurement signal MS is determined according to step S7. It may be particularly advantageous here to determine the rate of increase of the measurement signal MS after the second threshold value THD2 has been exceeded.

Then, in a step S23, the maximum value MAX_MS of the measurement signal MS of the post-cat oxygen sensor 37 is determined according to the procedure of step S8.

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In a step S24 an estimated value OSC of the current oxygen storage capacity of the three-way catalytic converter 22 is then determined according to step S10, after which in a step S26 a mass of fuel reduced on a one-time basis MFF_RED is
10 determined as a function of the gradient GRAD_MS of the measurement signal MS of the post-cat oxygen sensor 37 and/or the maximum value MAX_MS of the measurement signal MS and/or the estimated value OSC of the current oxygen storage capacity of the three-way catalytic converter 22. This takes place
15 analogously to step S11, preferably by means of one or more engine maps and preferably in such a way that, through the one-time reduction of the mass of fuel to be metered-in, after the one-time reduction of the mass of fuel to be metered-in has taken place, the three-way catalytic converter contains
20 approximately 50 % of the maximum amount of oxygen that can be stored there. Alternatively, in step S26, the mass of fuel reduced on a one-time basis MFF_RED can be permanently predefined.

25 In a step S27 the counter j is re-initialized with the value 1. Processing is then continued in step S5.

The mass of fuel to be metered-in on a one-time basis MFF_ADD can be metered in either during one operating cycle of the
30 relevant cylinder Z1 - Z4 in addition to the mass of fuel MFF or also distributed over several operating cycles of the cylinder Z1 - Z4. Alternatively, moreover, in block B5 the mass of fuel to be metered-in MFF can also merely be multiplied by the lambda control factor LAM_FAC and then, if

necessary, the mass of fuel to be metered-in on a one-time basis MFF can be added to this product or the mass of fuel to be reduced on a one-time basis MFF_RED can be subtracted. The mass of fuel reduced on a one-time basis MFF_RED can also be
5 set within one operating cycle of the relevant cylinder Z1 - Z4 or over several operating cycles. In addition, and this also applies to the mass of fuel to be metered-in on a one-time basis MFF_ADD, it can also be metered in or reduced in a distributed manner over a plurality of injection valves
10 assigned to different cylinders Z1 - Z4.